

CHAPLYGINA, Z.A.; ZHILYAYEVA, R.V.; TEODOROVICH, V.P.

Immunogenesis in experimental animals following the introduction of polyvinol, a blood-substituting solution. Zhur. mikrobiol., epid. i imm. 41 no. 2:142-143 F '64. (MIRA 17:9)

1. Leningradskiy institut perelivaniya krovi.

CHAPLYUK, M.I., aspirant; LAVROVA, I.G., assistant

Study of morbidity with temporary loss of working capacity. Sov.  
sdrav. 15 no.3:22-26 My-Je '56. (MLRA 9:8)

1. Iz kafedry organizatsii sdravookhraneniya (sav. - dotsent S.V.  
Kurashov) I Moskovskogo ordena Lenina meditsinskogo instituta.

(VITAL STATISTICS,

morbidity with temporary loss of working capacity (Rus))  
(WORKING,

capacity loss in morbidity statist. (Rus))

CHAPLYUK, M.I.; BASSALYK, D.A.

All-Russian conference of directors of higher medical schools,  
institutes of post-graduate medical training, and research institutes.  
Zdrav. Ros. Feder. 4 no.8:35-38 Ag '60. (MIRA 13:9)  
(MEDICINE—STUDY AND TEACHING)

CHAPLYUK, M.I. (Moskva)

Incidence disease among workers of the aniline dye industry. Zdrav.  
Ros. Feder. 4 no. 10:23-26 0 '60. (MIRA 13:10)

(CHEMICAL WORKERS—DISEASES AND HYGIENE)

(COAL-TAR PRODUCTS—TOXICOLOGY)

CHAPLYUK, M.I.; BASSALYK, D.A.

All-Russian conference of directors of advanced medical schools,  
post-graduate medical institutes and research institutes. Sov.med.  
25 no.8:148-150 Ag '60. (MIRA 13:9)  
(MEDICINE—CONGRESSES)

*Chapnik I.M.*  
USSR/Electronics - Gas Discharge and Gas-Discharge Instruments, H-7

Abst Journal: Referat Zhur - Fizika, No 12, 1956, 35161

Author: Chapnik, I. M.

Institution: None

Title: On the Theory of the Stratified Positive Column

Original

Periodical: Dokl. AN SSSR, 1956, 107, No 4, 529-532

Abstract: The nonlinear equations for longitudinal oscillations of plasma, proposed by Granovskiy and generalized by the author, are used to obtain equations that relate the discharge parameters with the length of the period and the attenuation of the positive column in a stratified state. The problem is solved for the one-dimensional case and in a linear approximation (no account is taken of the change of the parameters of the discharge along the radius of the tube). The expressions obtained for the length, for the periodicity, and for the decrement of attenuation are in agreement with experiment. Bibliography, 11 titles.

Card 1/1

AUTHOR  
TITLE

CHAPNIK I.M.

PA - 3550

The Theory of the Stratified Positive Column in the case of a Predominance of Volume Recombination.

(Teoriya sloistogo polozhitel'nogo stolba v sluchaye preobladayushchey ob'yemnoy rekombinatsii.- Russian)

PERIODICAL

Zhurnal Tekhn. Fiz 1957, Vol 27, Nr 5, pp 978-980 (U.S.S.R.)

ABSTRACT

In the course of the preceding work (Doklady Akademii Nauk SSSR 1956, Nr 4, p 107) this theory was suggested, but on this occasion volume recombination was neglected. In the present case, however, the case is investigated on which volume recombination is the predominant process in connection with the vanishing of charged particles. In some cases such circumstances may actually occur. The system of equations is again written down, but, in contrast to the previous work, the densities  $n_e$  and  $n_p$  are here assumed as constant according to the cross section of the tube. The linearization of the system of equations, like in the case of that in the previous paper, leads to a further system of equations of the amplitudes

$\bar{v}_e, \bar{v}_p, \bar{\epsilon}_e$  of the slight deviations from the steady solution.

In conclusion, equations for the periodicity length and for

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PA - 3550

The Theory of the Stratified Positive Column in the case of a Predominance of Volume Recombination.

the decrement of the dying down  $\delta$  are derived. From these two equations it is seen that in the case under investigation a periodic solution must always exist; the cathode end of the positive column serves as the place where stratification develops. The layers of the kind such as are obtained here are much closer than the "ordinary" layers and do not obey the law of similarity. The formula for the length of periodicity is here derived for ions with very low degree of mobility. The distance between the layers must in this case decrease with gas pressure, and this must occur more rapidly than is the case with "ordinary" layers.  
(With 7 Slavic references.)

ASSOCIATION: not given.  
PRESENTED BY: -  
SUBMITTED: 23.7. 1956  
AVAILABLE: Library of Congress.

CARD 2/2



**AUTHOR:**

Chapnik, I. M.

SOV/56-34-6-17/51

**TITLE:**

On the Mechanism of the Appearance of Striations in the Positive Column of a Gas Discharge (O mekhanizme vozniknoveniya sloistosti v polozhitel'nom stolbe gazovogo razryada)

**PERIODICAL:**

Zhurnal eksperimental'noy i teoreticheskoy fiziki, 1958, Vol. 34, Nr 6, pp. 1496-1503 (USSR)

**ABSTRACT:**

The purpose of this paper is the explanation of the following mechanism of the appearance of the striations: In the regions of the discharge which lie on the boundaries of the positive column (for instance, in the Faraday (Faraday) dark space) the values of the average energy of the electrons, of the potential gradient and of other quantities may be different from those values which under given conditions are found in the positive column. Besides of a solution independent of the coordinate  $x$  (the  $x$  axis is parallel to the column) the equations of the electronion plasma have still solutions which are equal to the sum of the solution independent of the coordinate  $x$  and of the oscillating function  $U_e(p, x) = U_{ec}(p) + \xi(p, x)U_{ec}(p)$ .  $U_e$  denotes the electron energy and  $U_{ec}$  the average energy of the electrons.

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SOV/56-34-6-17/51

On the Mechanism of the Appearance of Striations in the Positive Column of a Gas Discharge

The corresponding boundary conditions which take into account the discontinuity of the parameter on the boundary may be satisfied only by the periodic solution  $U_{ec} + \xi U_{ec}$ . In the systems of equations which are discussed in this paper the adhesion processes of the electrons to the gas molecules the recombination in the volume and the step ionization (stupenchataya ionizatsiya) are not taken into account. The calculations are discussed step by step. A diagram shows the obtained solutions of the "reestablishing force" and of the "potential energy" of the system discussed in this paper. The elastic force is rigid for the positive deviations of the electron energy and soft for the negative aberrations. The author reports also on a mechanical analogon of this system. One may change the form of the positive column (for instance make appear or disappear the striations) by introducing a probe (zonda) into the corresponding part of the column. The author thanks N. N. Bogolyubov, Member, Academy of Sciences, USSR, for the examination of this paper; V. L. Granovskiy, Professor; Ya. P. Terletskiy, Professor and A. A. Zaytsev for the discussion of the results and for

Card 2/3

SOV/56-34-6-17/51  
On the Mechanism of the Appearance of Striations in the Positive Column of  
a Gas Discharge

useful remarks. There are 3 figures and 16 references, 9 of  
which are Soviet.

ASSOCIATION: Moskovskiy gosudarstvennyy universitet (Moscow State University)

SUBMITTED: November 27, 1957

Card 3/3

30025  
S/020/61/141/001/007/021  
E104/B138

24,2140 (1160, 1164, 1182)

AUTHOR: Chapnik, I. M.

TITLE: Possible criteria of superconductivity

PERIODICAL: Akademiya nauk SSSR. Doklady, v. 141, no. 1, 1961. 70 - 73

TEXT: Studies on the properties of various superconductors have been reviewed in order to establish the following criteria for the origin of superconductivity: The hole concentration must be sufficiently high

( $N_p > 10^{19} \text{ cm}^{-3}$ ); the minimum interatomic distance must be limited to the range between 2.6 - 2.9 and 4kX, and there must be no ferromagnetism or strong paramagnetism. The author proves this criterion by a discussion of special results of other scientists. The change in  $T_s$  during

compression and stretching of superconductors can be explained by these criteria (B. Lazarev, L. Kan, ZhETF, 14, 463 (1944); N. Ye. Alekseyevskiy, ZhETF, 10, 746 (1940)). The increase of  $T_s$  obtained by plastic deformation can be eliminated by annealing (G. Minnigerode, Zs. Phys., 154.

Card 1/2

30025

S/020/61/141/001/007/021  
B104/B138

Possible criteria of ...

442 (1959). The mobility in superconductors is higher than in non-superconductors (I. Kikoin, B. Lazarev, ZhETF, 3, 44 (1933)). Mo, Ir, and Sb become superconductive by deformation (D. Shenberg, Sverkhprovodimost' (Superconductivity), 1955; A. Shal'nikov, ZhETF, 10, 630 (1940); W. Buckel, Zs. Phys. 154, 474 (1959)). The anomaly shown by Tl during strong compression is attributed to an increase of  $N_p$  in consequence of the appearance of a disordered lattice (L. Kan, B. Lazarev, A. Sudovtsev, DAN, 69, 173 (1949)). There are 4 tables and 21 references: 11 Soviet and 10 non-Soviet. The three most recent references to English-language publications read as follows: W. Pearson, Handbook of Lattice Spacings and Structures of Metals and Alloys, 1958; R. Hein, Phys. Rev., 102, 1511 (1958); B. Matthias, V. Compton, H. Schull, E. Correnzwit, Phys. Rev., 115, 1597 (1959).

ASSOCIATION: Novosibirskiy gosudarstvennyy universitet (Novosibirsk State University)

PRESENTED: June 1, 1961, by I. K. Kikoin, Academician

SUBMITTED: February 1, 1961  
Card 2/2

L 53684-65 EWT(1)/EPA(2)-2/EPA(2)-2/EEC(t)/EWA(m)-2 Pab-10  
 ACCESSION NR: AP5012339 UR/0288/65/000/001/0081/0090

AUTHOR: Chapnik, I. M.

TITLE: Mechanism for layer generation within a gas discharge 21

SOURCE: AN SSSR, Sibirskoye otdeleniya. Izvestiya. Seriya tekhnicheskikh nauk,  
 no. 1, 1965, 81-90

TOPIC TAGS: positive column layer theory, discharge layer generation, moving  
 gas discharge layer, gas discharge, Schottky theory, stratified discharge column

ABSTRACT: In spite of the recent suggestions of numerous researchers (see, e.g., G. Francis, Handbuch der Physik, Bd. 22, Tl 2, B. Springer, 1956; V. I. Gaponov, Elektronika, Part I, M., Fizmatgiz, 1960; Bito Janos, Magyar fiz. faliorat, 1962, 10, 303), the author considers the positive stratified column to be a solved enigma and develops the theory of the stratified discharge column as a generalization of the Schottky theory of the homogeneous column. The exposition is based on previous papers by the same author (I. M. Chapnik, Dokl. AN SSSR, 1956, 107, 529; Zh. tekhn. fiz., 1957, 27, 978; Zh. eksperim. i teor. fiz., 1958, 34, 1496). It covers the mechanism of production of stationary layers, the

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L 53684-65

ACCESSION NR: AP5012339

moving layers, and the double layer. The article concludes with an extended pictorial interpretation of the underlying events. Orig. art. has: 19 formulas, 6 figures, and 1 table.

ASSOCIATION: Novosibirskiy elektrotekhnicheskii institut (Novosibirsk Electrical Engineering Institute)

SUBMITTED: 29Feb64

ENCL: 00

SUB CODE: ME

NO REF SOV: 018

OTHER: 023

*BAB*  
Card

2/2

CHAPNIK, V.B.

Reorganization of production lines. Shvein.prom. no.2:8-10  
Mr-Ap '62. (MIRA 15:4)  
(Leningrad--Clothing industry) (Assembly-line methods)



CHAPNIK, Ye.I.

Combinations such as "stone wall" and "Moscow students" in modern English. Uch. zap. RGPI 22:27-43 '61. (MIRA 17:4)

247700

37925  
S/181/62/004/005/009/055  
B102/B138

AUTHORS: Vavilov, V. S., Smirnova, I. V., Chapnin, V. A.

TITLE: The interaction of lithium atoms introduced into silicon with the radiation defects of the structure

PERIODICAL: Fizika tverdogo tela, v. 4, no. 5, 1962, 1128-1131

TEXT: The authors studied the interaction of Li impurity atoms in Si single crystals with the structural defects that were produced by fast-electron bombardment. The Li impurity was introduced by diffusion from a Sn-Li melt containing 0.2 - 1% Li. Li equilibrium concentration in Si was reached at 550-650°C. The Li samples were p-type ( $\rho \sim 150 \text{ ohm}\cdot\text{cm}$ ) and cut out of single crystals. After introduction of Li the p-type samples were transformed to n-type with carrier concentrations of  $3 \cdot 10^{14} - 10^{16} \text{ cm}^{-3}$ . Since Li formed oxide ions  $\text{LiO}^+$ , which have shallow donor levels and are relatively stable at room temperature, the carrier concentration (n) equals the sum of the ions  $\text{Li}^+ + \text{LiO}^+$ . Electron bombardment (0.9 Mev) took place at room temperature. At Li concentrations

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The interaction of lithium atoms ...

S/181/62/004/005/009/055  
B102/B138

of  $3 \cdot 10^{14} - 5 \cdot 10^{15} \text{ cm}^{-3}$  two level groups were found in the upper half of the forbidden band:  $E_c - 0.17$  and  $0.4$  ev. For the level  $E_b$  which is filled with electrons  $E_b = 0.17$  ev is found. When the irradiated samples are heated to  $330-350^\circ \text{K}$  the carrier concentration was found to be greatly reduced. The results, presented by a curve, which has three sections, can be described by

$$\frac{n}{n_0} = A e^{-\frac{t}{\tau_1}} + B e^{-\frac{t}{\tau_2}} + C e^{-\frac{t}{\tau_3}} \quad (1).$$

$\tau_1 < \tau_2 < \tau_3$

The effective diffusion coefficient  $D_{\text{eff}} = 0.1\% D_0$ ,  $D_0$  is the diffusion coefficient of Li when O is absent. There are 2 figures.

ASSOCIATION: Moskovskiy gosudarstvennyy universitet im. M. V. Lomonosova (Moscow State University imeni M. V. Lomonosov)

SUBMITTED: December 8, 1961

Card 2/2

VAVILOV, V. S.; SMIRNOVA, I. V.; CHAPNIN, V. A.

"On Defects Introduced by Fast Electrons into Silicon Doped by Lithium"

Paper was submitted at the International Conference on  
Crystal Lattice Defects at Kyoto, 7-12 Sep '62

(for Vavilov, v. s.) P. N. Lebedev Inst. of Physics  
Leninsky, Prospect 53, Moscow

L 8938-66 EWT(1)/EWT(m)/EWP(t)/EMP(b) IJP(c) JD  
 ACC NR: AP5026856 SOURCE CODE: UR/0170/65/009/004/0536/0537

AUTHOR: Chapnin, V. A. 51

ORG: Physics Institute im. P. N. Lebedev, Moscow (Fizicheskiy institut) 51 23

TITLE: Joule heating of germanium and gallium arsenide in liquid nitrogen 51 23

SOURCE: Inzhenerno-fizicheskiy zhurnal, v. 9, no. 4, 1965, 536-537 27

TOPIC TAGS: germanium, arsenide, gallium compound, Joule law, electric resistance 21, 44, 55

ABSTRACT: The article presents the results of a determination of the maximum dissipation power for germanium and gallium arsenide in liquid nitrogen. The samples were rectangular blocks of p-Ge and n-GaAs ( $p \sim 10^{14}/\text{cm}^3$ ,  $n \sim 10^{17}/\text{cm}^3$ ) with different surface areas ( $0.2-7.5 \text{ cm}^2$ ). The degree of heating up of the samples was determined from the form of the volt ampere characteristics, and from the dependence of the resistance and the temperature on the power evolved. At small powers up to 0.01 watts, the samples were at the temperature of liquid nitrogen and Ohm's law was obeyed. With a further increase in the power, the temperature of the samples increases up to 80-83 K, while the resistance also increases. The dissipation is determined from the lattice vibrations. In this region, the degree of heating is not

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UDC:536.7+536.78

L 8938-66

ACC NR: AP5026856

directly proportional to the surface area of the samples. When the critical power of  $13 \pm 3$  watts/cm<sup>2</sup> is reached, a sharp temperature jump takes place up to 100-120 K, the resistance jumps by 2-3 times (due to the decrease of the mobility), and the current falls. Again, when the critical power is reached, there are temperature jumps up to 400 K and the current increases. The presence of hysteresis in the volt ampere characteristics indicates that the power necessary for the appearance of a temperature jump is less than the power required for maintaining a "punctured" state. Analogous results were obtained for gallium arsenide. However, on attainment of the critical power of 13 watts/cm<sup>2</sup> the temperature increases suddenly up to approximately 450 K (this is connected with the constant nature of  $n$  and  $\mu$  in the interval from 80 to 450 K). The coincidence of the critical powers for germanium and gallium arsenide proves that the temperature jumps are connected with the behavior of liquid nitrogen, in particular, with the formation of a gas jacket around the sample and a decrease in heat transfer. The significant degree of heating up of the samples at low powers is evidently connected with the superheating of the liquid phase, as well as with a decrease in heat conductivity with a rise in temperature. Orig. art. has: 2 figures.

SUB CODE:IC, MM/ SUBM DATE: 09Feb65/ ORIG REF: 003/ OTH REF: 001

Card 2/2

44163

S/181/62/004/012/003/052  
B104/B102

24/580

AUTHORS: Smirnova, I. V., Chapnin, V. A., and Vavilov, V. S.

TITLE: Radiation defects in lithium-doped silicon

PERIODICAL: Fizika tverdogo tela, v. 4, no. 12, 1962, 3373-3380

TEXT: The effect of lithium on the formation of stable radiation defects in silicon and on the annealing of these defects is studied by determining the temperature dependence of the carrier concentration from the Hall effect. The lithium was introduced into Si single crystals by diffusion annealing (550-650°C) from a tin-lithium alloy. The single crystals had a resistivity of 100 ohm·cm; after doping they had n-type conductivity. The carrier concentration lay between  $3 \cdot 10^{14}$  and  $2 \cdot 10^{17} \text{ cm}^{-3}$ . The specimens were irradiated by 0.9-Mev electrons at room temperature. Results: In n-type silicon with lithium up to concentrations of  $(1-2) \cdot 10^{17} \text{ cm}^{-3}$ , shallow energy-levels arise in the range from 0.06 to 0.14 ev below the bottom of the conduction band, which are related to primary radiation defects, e.g., to pairs of interstitial atoms and

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Radiation defects in ...

S/181/62/004/012/003/052  
B104/B102

vacancies which are separated by different distances. The lithium in the Si crystal interacts with these defects. Such interaction is similar to the processes that occur during the annealing of genetically unrelated vacancies and interstitial atoms. The trapping radius has the same order as the lattice constant, ( $r_{\min} = 5.4 \cdot 10^{-8}$  cm). In crystals that, after part of the lithium has been deposited in the defects, are again of p-type conductivity, the levels 0.45 ev, 0.28 ev and 0.21 ev were observed above the top of the valency band. The centers corresponding to the level  $E_v + 0.28$  ev did not disappear completely even during annealing for several hours at  $450^\circ\text{C}$  and above; those corresponding to the level  $E_v + 0.21$  ev disappeared completely during annealing at  $450^\circ\text{C}$ . There are 4 figures.

ASSOCIATION: Moskovskiy gosudarstvennyy universitet im. M.V. Lomonosova  
(Moscow State University imeni M.V. Lomonosov)

SUBMITTED: June 16, 1962

Card 2/2



38524-65 EPP(c)/EPA(w)-2/EWT(1)/EWT(m)/EWP(b)/T/EWA(m)-2/EWP(t) Pr-4/Fab-10  
IMP(c) RM/JD

ACCESSION NR: AP5005292

S/0181/65/007/002/0506/0512

AUTHOR: Chapnin, V. A.

TITLE: Impact ionization in germanium doped with zinc

SOURCE: Fizika tverdogo tela, v. 7, no. 2, 1965, 506-512

TOPIC TAGS: germanium, doping, impact ionization, electric breakdown, carrier phonon interaction

ABSTRACT: The article deals with impact ionization of zinc in germanium. The impurity level  $E_i = 0.009$  eV. The experiments were made at temperatures 4.2--20.4 K. The breakdown voltage was measured with a DEBO-1 oscilloscope. Some 50 samples with effective acceptor density between  $2.0 \times 10^{14}$  and  $2.0 \times 10^{16}$  cm<sup>-3</sup> and with zinc-atom density  $4 \times 10^{14}$  to  $4 \times 10^{17}$  cm<sup>-3</sup> were investigated. The results show that the breakdown field rises to  $1.5 \times 10^3$  V/cm in the interval 4.2--20.4 K and rises to  $6 \times 10^3$  V/cm at 20.4 K.

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ACCESSION NR: AP5005292

temperature. It is also established that the breakdown field is practically independent of the effective concentration of the acceptors in the interval  $10^{14}$  to  $2 \times 10^{16} \text{ cm}^{-3}$ . The results are interpreted on the basis of the theory of impact ionization with account of the interaction between the carriers and the acoustic and optical phonons. "The author thanks V. A. Chuyenkov for interest and discussion of the results and V. I. Kononenko for help with the work." Engl. art. has: 4 figures, 10 formulas, and 2 tables.

ASSOCIATION: Fizicheskiy institut im. P. N. Lebedeva AN SSSR, Moscow (Physics Institute, AN SSSR)

SUBMITTED: 29Jul64

ENCL: 00

SUB CODE: SS,GC

NR REF SOV: 009

OTHER: 008

Card 2/2

L 21229-66 EWT(m)/I/EWP(t) IJP(c) JD  
ACC NR: AP6003804 SOURCE CODE: UR/0181/66/008/001/0256/0253

AUTHORS: Vul, B. M.; Chapnin, V. A.

ORG: Physics Institut im. P. N. Lebedev AN SSSR, Moscow  
(Fizicheskii institut AN SSSR)

TITLE: Interaction between lithium and lattice defects in cadmium  
telluride <sup>27</sup> <sub>44-55, 15</sub>

SOURCE: Fizika tverdogo tela, v. 8, no. 1, 1966, 256-258

TOPIC TAGS: lithium, cadmium telluride, crystal lattice defect,  
impurity level, drift mobility, valence band, capture cross section,  
radiation damage

ABSTRACT: The authors obtained low-resistance p-type CdTe by dif-  
fusion of lithium from the vapor phase in high-resistance p-type  
CdTe at 900C in saturated vapor of cadmium. The lithium produces in  
the CdTe a shallow acceptor level. The lithium was found to have a  
high mobility even at room temperature, so that it cannot be used to  
produce a pn junction. A reason for this phenomenon is the inter-

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L 21229-66

ACC NR: AP6003804

action between the lithium and the lattice defect present in the cadmium telluride as a result of deviation from stoichiometry. This phenomenon is similar to that previously observed for interaction between lithium and radiation defects in silicon. Because of its high mobility the lithium migrates to the crystal and when it encounters defects it attaches itself to them in the form of neutral atoms, capturing holes from the valence band. The accompanying change in the resistance was measured at several temperatures and the results are plotted. It is deduced that the diffusion coefficient of lithium should be less than approximately  $10^{-14}$  cm<sup>2</sup>/sec at 60C. It is concluded that this phenomenon can be used to control the degree of perfection of crystals and also to heal radiation defects at relatively low temperatures. Orig. art. has: 2 figures and 1 formula.

SUB CODE: 20/ SUBM DATE: 27Jul65/ ORIG REF: 002/ OTH REF: 001

Card 2/2 *ddw*

L 42811-66 EWT(m)/T/EWP(t)/ETI IJP(c) JD/JH

ACC NR: AP6026706

SOURCE CODE: UR/0181/66/008/008/2466/2467

AUTHOR: Chapnin, V. A.

ORG: Physics Institute in. P. N. Lebedev, AN SSSR, Moscow (Fizicheskiy institut AN SSSR)

TITLE: A luminescent cadmium telluride diode

SOURCE: Fizika tverdogo tela, v. 8, no. 8, 1966, 2466-2467

TOPIC TAGS: luminescent material, cadmium telluride, optic material

ABSTRACT: The author describes a luminescent surface-barrier CdTe diode. The diodes were made with n-CdTe with a carrier concentration  $\sim 10^{14} \text{cm}^{-3}$  and mobility of  $\sim 1.2 \times 10^3 \text{cm}^2/\text{v-sec}$  at 300K. Al was introduced into the initial material by diffusion at 800C in saturated cadmium vapors. As a result of diffusion, the carrier concentration rose to  $5 \cdot 10^{16} \text{cm}^{-3}$  and mobility dropped to  $1 \cdot 10^3$ . Contacts (indium on one side and gold on the other) were deposited on CdTe plates, which were then heat treated at 300C for 30 min in a vacuum. Recombination radiation was observed in the direction parallel to the p-n junction plane with linear voltage application. The volt-ampere characteristics of the diodes are normal and maintain voltage in the reverse direction up to 20 v. Diode resistivity in a linear direction is  $\sim 50\text{--}100 \text{ohm}$  at 300K and it drops somewhat at 80K. The relationship  $c^{-2}=f(u)$  is in a majority of cases linear; however, for some specimens saturation of capacities occurs at voltages

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L 42811-66

ACC NR: AP6026706

above 5 v. In conclusion, the author expresses his gratitude to B. M. Vul for critical comments, and to S. A. Medvedev and S. N. Maksimovskiy for the materials presented. Orig. art. has: 1 figure. [26]

SUB CODE: 20/ SUBM DATE: 28Jan66/ ORIG REF: 002/ OTH REF: 004/ ATD PRESS: 5067

Cord 2/2

CHAPNITSKIY, L. A.

Cost accounting for construction work in the building associations Moskva, Gos.  
izd-vo stroit. lit-ry, 1950. 111 p. (Biblioteka stroitel'ia po voprosam ekonomiki i  
planirovaniia) (51-15253)

HF5686.B7C48

CHAPNITSKIY, I. I.

A

Uchet i kal'kulirovaniye stoimosti stroitel'nogo proizvodstva (Accounting and calculation of value of the construction output) lzd. 2 dopol i perer. Moskva, Gos. lzd-vo Lit. po Stroitel'stvu i Arkhitekture, 1952. 171 p. tables.

N/5

748.161

.C4

1952



CHAPO, ELEK

B. T. A.  
V. 3 No. 3  
Mar. 1954  
Metals- Heat  
Treatment

3771\* Gaseous Annealing of Malleable Castings. (Hungarian.) Elek Chapó. *Outside*, v. 4, no. 8, Aug. 1953, p. 165-170. Various reactions involved in annealing white cast iron are discussed. Describes effect of gas atmosphere upon decarburization and graphitization; influence of H in furnace atmosphere, and effect of Mn-S ratio of Fe upon annealing rate. Table, graphs. (To be continued.)

CHAPD, E.

B. T. R.  
Vol. 3 No. 4  
Apr. 1954  
Metals-Heat Treatment

5319\* Annealing in a Gaseous Atmosphere. III. (Hungarian.) Elek Clapó. *Ontde*, v. 4, no. 9, Sept., p. 185-189. Describes structure and operation of annealing furnaces. Advantages of annealing in a gaseous atmosphere are reviewed. Diagrams, table. 9 ref.

76. The effect of chromium and boron on the quality of malleable cast iron — *A krom és bor hatás a temper-  
mentált öntvény minőségére* — P. Chard. (Foundry — Kőhízási  
Lapok, Budapest — Vol. 2-1934-1935, pp. 25-30, 16 figs.,  
3 tabs.)

The combined effect of chromium and boron on the production of malleable cast iron was investigated in order to eliminate the harmful effect of chromium contained in the scrap added to the charge. Experiments were also

conducted on an industrial scale with malleable cast iron for the manufacture of fittings. It was found that a 0.0015% boron content had a slight stabilizing effect on carbides, a higher percentage had an increased graphitizing effect. Boron in a thousandth per cent order probably has a great graphitizing i.e. nucleus-forming effect. Due to its stabilizing properties in carbide the interval of carbide decomposition is somewhat increased while the interval of pearlite decomposition is more effectively reduced. Assuming an identical period of heat treatment boron has a detrimental influence on strength properties, the strength properties of black-heart malleable cast iron, contaminated with chromium but alloyed with boron, are identical with those of white-heart malleable cast iron. In case of 0.08 to 0.1% chromium content treatment with 0.003 to 0.003% boron is the most advantageous.

CHAPU, F.  
 Condition for the Production and Quality Properties of  
 Nodular Grey Cast Iron. F. Varga, B. Kertész, E. Csontos,  
 K. Jánosy, and J. Sándor. (Köveskút Lapok, 1969, 9, Aug.,  
 168-192; Sept., 193-211). The development of nodular grey  
 iron production in Hungary and other countries is reviewed.  
 Numerous experiments in the Hungarian Iron and Steel  
 Research Institute confirm the principle that a successful  
 inoculation depends both on the low carbon content and on  
 the superheating of the melt. An increasing steel and  
 content in the charge decreases the carbon content in the  
 melt. Simultaneously an increase in tensile strength was  
 observed in case of properly performed inoculations. The  
 inoculation effect of  $\text{CaSi}$  has always been found better than  
 that of  $\text{FeSi}$ . -Z, x.

706  
 100



VARGA, Ferenc; KOROS, Bela; CHAPO, Elek; JANOSSY, Kazmer; SIMA, Rezsó

Manufacturing conditions and properties of modified cast  
iron. Pt. 2. Koh lap 9 no. 9: Supplement: Ontode 5 no. 9:  
193-208 S '54.

CHAPO, Elek

Effect of chromium and boron on the quality of malleable cast iron. Koh lap 9 no. 2: ~~Supplement~~: Ontode 5 no. 2: 25-30 F '54.

1. Vasipari Kutato Intezet.

CHAPO, Elek, okleveles gepeszmernok

Significance of slag control in iron foundries. Koh lap 12  
no. 11/12 Supplement: Ontode 8 no. 11/12 237-242 N-D '57.

1. "Kohaszati Lapok" szerkeszto bizottsagi tagja.



CHAP0, E.

The importance of slag control in iron foundries.

P. 237. (ONTODE.) (Budapest, Hungary) Vol. 7, No. 11/12, Nov./Dec. 1957

SO: Monthly Index of East European Accession (EEAI) LC. Vol. 7, No. 5, 1958

CHAPO, E., Koros, B., Kollar, K.

Evaluating the average life of ingot molds in steel factories by means of mathematical analysis. p. 20.  
(ONTODE, Vol. 8, no. 1/2, Budapest, Hungary)

SO: Monthly List of East European Accessions (BEAL) LC. Vol.6, no. 12, Dec 1957.  
Uncl.

CHAP0, E.

W. Kamekichi's "Japanese Iron Production", a review of an article.

p. 262. (KOHASZAT LAPOK) Vol. 12, no. 6, June 1957  
Budapest, Hungary

SO: Monthly Index of East European Accessions (EEAI) LC, Vol. 7, No. 3,  
March 1958

CHAPO, E.

TECHNOLOGY

PERIODICAL: KOHASZATI LAPOK, Vol. 13, no. 7, July 1958

Chapo, E. Development of manufacturing malleable cast iron in Hungary and abroad. p. 152.

Monthly list of East European Accessions (EEAI) LC, Vol. 8, No. 2,  
February 1959, Uncl<sub>ss</sub>.

CHAPO, Elek

Report on the 9th general meeting of the Institute of Indian Foundrymen. Koh lap 93 no.1:Suppl: Ontode 11 no.1:18 Ja '60.

1. "Kphaszati Lapok" szerkeszto bizottsagi tagja.

CHAPÓ, Elek, okleveles gépészmérnök

Gas-phase annealing experiments. Koh lap 93 no.3:Suppl: Ontode 11  
no.3:49-55 Mr '60.

1. Vasipari Kutató Intézet; "Kohászati Lapok" szerkesztő bizottsági  
tagja.

CHAPO, Elek

Announcement of a contest. *Moh* lap 95:Suppl.:Ontode 13 no.6:  
143 Je '62.

1. Országos Magyar Banyászati és Kohászati Egyesület Bíráló  
Bizottsága elnöke.

CHAPO, Elek, okleveles gepeszmernok

Crack detection on thin-walled castings. Koh lap 97 no.11: ~~241-249~~  
Okt. 15 no.11: 241-249 N '64.

1. Iron Industry Research Institute, Budapest, and Editorial board member, "Kohasziati Lapok."



Chapo, Nemesh

RUMANIA/Soil Science. Genesis and Geography of Soils.

I-2

Abs Jour: Referat Zh-Biol., No 6, 25 March, 1957, 22427.

Author : Chapo. Nemesh

Inst :

Title : Nomenclature and Classification of Soils in Transylvania.

Orig Pub: Studii si cercetari stiint. Acad. R.P.R. Fil. Cluj, 1954,  
ser. 2, 5, No 3-4, 201-220

Abstract: Names of soils must reflect the basic physico-chemical and biological processes which occur in those soils under the influence of cultivation, fertilization, etc. An example is given of division of the Rumanian People's Republic's principal soils into types, subtypes, groups and varieties. The suggested classification of the Republic's soils, particularly Transylvania's, is made by taking into account the climatic peculiarities of the territory, soil-forming types, and the character of the vegetative cover. A delineation of Panon, Karpát, Dak and Pont soil provinces within

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-2-

RUMANIA/Soil Science. Genesis and Geography of Soils.

I-2

Abs Jour: Referat Zh-Biol., No 6, 25 March, 1957, 22427

the Republic's borders is suggested. The scheme of soil classification of Transylvania and the Rumanian People's Republic is given. The studies were carried out in the agronomical institute of Glyui.

Card : 2/2

-3-

RADNOT, M.; ROSLAVTSEV, A.V., prof.; SIZA, Mario, doktor [translator];  
VEYNSHTEYN, P., doktor med. nauk, nauchnyy red.; CHAPODI, I., doktor  
med. nauk, nauchnyy red.; BERNAT, D'yerd', otv. izd.; ERDI, K., otv.  
red.; CERGE, I., tekhn. red.

[Atlas of eye diseases] Atlas glaznykh boleznei. Budapest, Izd-vo  
Akad. nauk Vengrii. Vol.1. 1962. 188 p. (MIRA 15:1)

1. Chlen-korrespondent AN Vengrii (for Radnot). 2. Direktor moskov-  
skogo instituta glaznykh bolezney in. Gel'mgol'tsa (for Roslavitsev).  
(EYE—DISEASES AND DEFECTS)  
(ANATOMY, PATHOLOGICAL—ATLASES)

CHAPOROVA, I. N.										1ST AND 2ND GROUPS										1ST AND 2ND GROUPS									
5										19																			
<p><b>Preparation of Polished Sections and the Revelation of the Microstructure of Metals-Quenched Solid Alloys. I. N. Chaporova. (Zavodskaya Laboratoriya, 1940, vol. 18, July, pp. 788-806). [In Russian].</b> Methods are described which have been proved satisfactory for the preparation of sections of solid alloys, based on tungsten carbide, for the study of microstructure. Sections were prepared with the aid of a rotating carborundum disc, followed by preliminary polishing with boron tungstate powder wetted with paraffin. For further preliminary polishing, two sizes of alcohol-wetted diamond dust were used. Final polishing was carried out either with diamond dust down to 1 <math>\mu</math> particle size or with a suspension of alumina. The procedure for etching the polished sections and for identifying the microstructures is described and tabulated, some photomicrographs of typical structures being shown.—a. z.</p>																													
<p>AS 15-15A METALLURGICAL LITERATURE CLASSIFICATION</p>																													
1ST AND 2ND GROUPS										1ST AND 2ND GROUPS										1ST AND 2ND GROUPS									
1ST AND 2ND GROUPS										1ST AND 2ND GROUPS										1ST AND 2ND GROUPS									

CHAPOROVA, I. N.

Metals

Ceramics

Microstructure

Techniques

Jul 49

"Preparation of Microsections and Exposing the Microstructure of Hard Metalloceramic Alloys," I. N. Chaporova, Moscow Combine for Hard Alloys, 7 pp

"Zavod Lab" No 7

Describes threefold process for preparing microsections of hard metalloceramic alloys (86-92R): sections of hard surface, microsectioning, and obtaining a flat surface, microsectioning, and polishing. Alloy consisted basically of tungsten

62/49183

Jul 49

Metals (Contd)

Extensive table shows results of using various etching fluids and etching conditions for specific cases. Includes microphotographs of the microstructure for these different cases.

62/49183

CHAPOROVA, I. N.

CHAPOROVA, I. N. - Author's abstract of a dissertation on the subject of an "Investigation of the process of formation of a solid solution from the interaction of tungsten carbide and titanium carbide in a mixture of powders", presented toward the academic degree of Candidate of Technical Sciences. Moscow, 1955. Min Higher Education USSR. Moscow Inst of Nonferrous Metals and Gold izeni M. I. Kalinin. (Dissertation for the degree of Candidate of Technical Science ).

SO: Knishnaya Letopis' No. 46, 12 November 1955. Moscow

AUTHORS: Vasil'yeva, N. P., Sultanyan, T. A., SOV/32-24-9-20/53  
Chaporova, I. N.

TITLE: The Method of Electron-Microscopic Examination of the  
Intragranular Structure of Pulverulent and Compact Tungsten  
(Metodika elektronnomikroskopicheskogo issledovaniya  
vnutrizerennoy struktury poroshkoobraznogo i kompaktnogo  
vol'frama)

PERIODICAL: Zavodskaya Laboratoriya, 1958, Vol 24, Nr 9,  
pp 1090 - 1092 (USSR)

ABSTRACT: In the present case an electron-microscopic method  
was employed for the examination of the submicrostructure  
of pulverulent and compact tungsten samples. The  
tungsten powder was obtained by a reduction from tungstic  
anhydride by means of hydrogen at 900° and 1200°. The  
synthetic material AKR-7 (emulsion polymethyl metha-  
crylate) was employed as binder for the powder and a  
mixture of a 20% potassium ferricyanide solution and  
caustic potash solution served as etching agent in  
order to obtain the structure mentioned in the title.  
It was found that titanium replicas are best suited

Card 1/2

The Method of Electron-Microscopic Examination of the SOV/32-24-9-20/53  
Intragranular Structure of Pulverulent and Compact Tungsten

to reproduce the submicrostructure. The most reasonable results were obtained at a vacuum of not less than  $10^{-4}$  mm Hg and a weighed sample of 0,008-0,009 g. The tungsten powder obtained at  $1200^{\circ}$  consists of granules with dimensions of 10 to  $200\mu$ . A decrease of reduction temperature to  $800^{\circ}$  -  $900^{\circ}$  entails a decrease of granules to  $1-2\mu$ . Pictures of the submicrostructures obtained and corresponding explanations are given. There are 3 figures and 2 references, which are Soviet.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov (All-Union Scientific Research Institute of Hard Alloys)

Card 2/2



AUTHORS: Svistunova, Z. V., Chaporova, I. N., SOV/32-24-9-21/53  
Vasil'yeva, N. P., Sultanyan, T. A., Kiselev, V. Ye.

TITLE: An Electron-Microscopic Investigation of the Structure of  
Powder-Metallurgical Hard Alloys (Elektronnomikroskopicheskoye  
issledovaniye struktury metallokeramicheskikh tverdykh splavov)

PERIODICAL: Zavodskaya Laboratoriya, 1958, Vol. 24, Nr 9, pp 1093-1095  
(USSR)

ABSTRACT: In this paper experimental results obtained by employing new  
methods of producing replicas for structural examinations of  
hard alloys are given. Furthermore, the conditions for  
polished section etching are determined. The polished sections  
of hard alloys of the types BK 6, BK 8, BK11, T15K6 and T3OK4  
were produced as usual, the method of polishing by etching  
being employed. The reagents used and the conditions are given  
in a table. It is observed that satisfactory results are  
obtained by titanium and collodion replicas. Quartz replicas  
have the disadvantage of being non-resistant. Among other  
facts the results mentioned show that the alloys of tungsten  
carbide with cobalt, a normal carbon content provided, consist

Card 1/2

An Electron-Microscopic Investigation of the Structure SOV/32-24-9-21/53  
of Powder-Metallurgical Hard Alloys

of two phases- the tungsten carbide and the solid solution  
of tungsten and carbon in cobalt. The fine-grained alloy  
BK consists of tungsten carbide granules of 0,4 to 0,7 $\mu$ .  
Pictures of the microstructures obtained are given.  
There are 4 figures, 1 table, and 8 references, 6 of which  
are Soviet.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh  
splavov (All-Union Scientific Research Institute of Hard  
Alloys)

Card 2/2

12.6100

SOV/180-59-5-14/37<sup>67802</sup>

AUTHORS: Chaporova, I.N., and Shchetilina, Ye.A. (Moscow)

TITLE: Solubility of Tungsten Carbide<sup>1</sup> in Cobalt<sup>2</sup> and Nickel<sup>1</sup>

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Metallurgiya i toplivo, 1959, Nr 5, pp 91-96 (USSR)

ABSTRACT: The author mentions the diversity of published opinions on the solubility limits of tungsten carbide WC in cobalt and nickel (Refs 1-8). The object of the present work was the more precise determination of the solubility in cobalt compared with that in nickel and the study of some of the properties of the solid solutions formed. Alloys were prepared from tungsten-carbide, cobalt and nickel powders (Table 1). For solubility determinations mixtures of cobalt with 2, 4, 6, 10, 12, 15, 18 and 20 weight % WC and of nickel with 6, 15, 18 and 20 weight % WC were prepared. Compacted cylinders 18 mm in diameter covered in graphite particles were reduced in a hydrogen stream at 700-800°C for 5 hours. Alloys were prepared by fusion and sintering for 1-2 hours at 1200-1450 °C in a laboratory vacuum furnace, followed by cooling in the furnace at about 200-300 °C per minute to 700-800 °C.

Card  
1/3

67802

SOV/180-59-5-14/37

**Solubility of Tungsten Carbide in Cobalt and Nickel**

Carburizing (to make good the C-deficiency of the WC preparation) sintering of specimens at 1250-1450 °C was effected in a current of hydrogen in contact with carbonaceous material. Microstructural investigation showed that the WC-Co alloys with under 12% WC contain a single phase (Fig 1) and those with over 12%, two (Fig 2). Carburizing treatment led to the appearance of lamellar graphite inclusions (2, 4 and 6% WC) and also (10, 12, 15 and 18% WC) a WC phase in a eutectic. Rapid cooling in water gave a WC + Co-phase + C eutectic at grain boundaries (Fig 3); cooling in the furnace gave the corresponding two binary eutectics. The author concludes that with excess carbon the solubility of WC in cobalt at the eutectic temperatures does not exceed 10 weight %. The authors' previous work (at VNIITS in 1954-56) indicates (Fig 4a) that a higher solubility is obtained with lower carbon contents. For the nickel alloys prepared by vacuum sintering at 1200-1425 °C rapid quenching was adopted. Fig 5 shows the absence of WC-phase particles and the presence of carbon inclusions in the 15% WC alloy vacuum melted at 1380 °C. Fig 6 shows

Card  
2/3

Solubility of Tungsten Carbide in Cobalt and Nickel <sup>67802</sup> SOV/180-59-5-14/37

individual crystals of WC and nickel-graphite eutectic in the 18% alloy vacuum melted at 1350 °C. In 15% alloys obtained under carburizing conditions no WC phase was detected. The authors conclude that the limiting solubility of WC in nickel in the presence of structurally free carbon is about 15 wt %. The results of X-ray investigation (including lattice-parameter determinations of cobalt) of WC-Co alloys are given in Table 2; they confirm those of microscopic examinations of the same samples. Fig 7 shows the lattice parameter of nickel in relation to the WC-content, the value rising from 3.517 for pure Ni to 3.545 Å for melted 20% WC alloy. Here too X-ray results confirm those of microscopic investigation. Microhardness determinations showed that with increasing WC-content and especially after the appearance of the WC-phase the microhardness rises. Fig 8 shows the microhardness vs WC-content for nickel; this was always less than that of the cobalt-base alloys. There are 8 figures, 2 tables and 8 references, of which 2 are Soviet, 5 English and 1 German.

Card  
3/3

SUBMITTED: May 22, 1959

**AUTHORS:** Shchetilina, Ye.A. (Engineer) and  
Chaporova, I.N. (Cand.Tech.Sci.)

SOV/129-59-6-5/15

**TITLE:** Interaction of Niobium Carbide with Cobalt  
(Vzaimodeystviye karbida niobiya s kobal'tom)

**PERIODICAL:** Metallovedeniye i termicheskaya obrabotka metallov,  
1959, Nr 6, pp 19-23 (+ 2 plates) (USSR)

**ABSTRACT:** For investigating the system Niobium Carbide - Cobalt, the specimens were produced by powder metallurgy methods from pulverized niobium carbide and cobalt. The chemical analyses of these materials are entered in Table 1, page 19. The specimens were placed in corundum crucibles which were put into graphite dishes and heated for two hours at 1250, 1300, 1320, 1340, 1350, 1375 and 1400 °C followed by rapid cooling (hardening) in the coolers (refrigerators) of the furnace. The specimens were sintered at 1225, 1450 and 1550 °C and during the tests temperature was controlled automatically with an accuracy of  $\pm 5^\circ\text{C}$ . Data on the state of the specimens after sintering and the results of microstructure investigations of some of these are entered in Table 2, page 20. In Figs 1-3 (plates)

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## Interaction of Niobium Carbide with Cobalt

SOV/129-59-6-5/15

microstructure photographs are reproduced of cobalt with various percentages of NbC. In Fig 4 the dependence is graphed of the linear shrinkage of the investigated alloys on the sintering temperature. In Fig 5 the dependence is graphed of the linear shrinkage as a function of the carbide content for the sintering temperatures 1250 - 1235 °C. In Fig 6 an approximate diagram of state of the system NbC-Co is reproduced, which is based on the data derived from the here-described investigations. On the basis of the data of the metallographic investigations and measurement of the shrinkage of the specimens during sintering, it was established that the eutectic appears for a NbC content of about 0.5 mol %. Consequently it can be assumed that the solubility of niobium carbide in cobalt at the fusion temperature of the eutectic does not exceed 0.5 mol %. This was also confirmed by X-ray data; the lattice parameters of pure cobalt and of the cobalt phase in the alloys containing 0.5 - 3 mol % NbC did not differ. Comparing the here-given data on the system NbC-Co with results of investigations

Card2/3

Interaction of Niobium Carbide with Cobalt

SOV/129-59-6-5/15

of the system TiC-Co published earlier (Ref 6), an analogy can be observed between the interaction of niobium carbides and of titanium with cobalt: both systems are eutectic in character, the maximum solubility in the solid state is approximately the same in both cases and the fusion temperatures and the composition of the eutectics also did not differ greatly.

There are 6 figures, 3 tables and 6 references, 5 of which are Soviet and 1 English.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov (All-Union Scientific Research Institute for Hard Alloys)

Card3/3



34704

S/137/62/000/002/049/144

A006/A101

15.2460

AUTHORS: Chaporova, I. N., Shchetilina, Ye. A., Serebrova, S. I.

TITLE: On the effect of the composition of carburizing phases on some mechanical properties of cermet WC-Co and WC-Ni sintered carbides

PERIODICAL: Referativnyy zhurnal, Metallurgiya, no. 2, 1962, 33, abstract 2G263 ("Sb. tr. Vses. n.-i. in-t tverdykh splavov", 1960, no. 2, 90-104)

TEXT: The authors studied the effect of the cooling rate on the composition of carburizing phases and the mechanical properties of WC carbides with 10 and 30% Co or Ni, differing by the C content. The C content varied depending on the initial composition of the charge and sintering conditions (filling, atmosphere). Slowly cooled carbides with 10% Co, independent of the C content, showed in all the experiments higher  $\sigma_{0.1}$  than rapidly cooled carbides. Carbides with 30% Co showed on the contrary higher strength in rapid rather than in slow cooling. Changes in hardness  $H_v$  of WC-Co and WC-Ni carbides cooled at various rates, were not revealed. WC-Ni carbides are less hard and durable than WC-Co carbides of an analogous composition. This difference is caused by different properties of pure metals and solid solutions of their base. No

Card 1/2

On the effect of the composition ...

S/137/62/000/002/049/144  
A006/A101

changes in the grain growth of the WC phase in alloys depending on the cooling rate were revealed. Data on  $H_v$  and  $\delta_{\text{H}}$  are presented depending on the sintering conditions and the C content in the carbides.

A. Epik

[Abstracter's note: Complete translation]

X

Card 2/2

S/180/61/000/001/011/015  
E021/E406

AUTHORS: Chaporova, I.N. and Shchetilina, Ye.A. (Moscow)  
TITLE: The Limits of the Single-Phase and Two-Phase Regions  
in the Tungsten-Carbon-Cobalt and Tungsten-Carbon-  
Nickel Systems ✓ ✓ ✓  
PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh  
nauk, Metallurgiya i toplivo, 1961, No.1, pp.126-132

TEXT: Results of studies of the limits of the single phase (Co or Ni) and two-phase (Co phase + WC or Ni phase + WC) regions are given. Alloys were made from powders of tungsten carbide, cobalt, nickel, and tungsten. All the samples after pressing were sintered at 650 to 700°C in a current of hydrogen. The alloys were further sintered in a laboratory vacuum furnace at temperatures of 1400 to 1450°C. Metallographic analysis was carried out. Alloys in the ternary W-C-Co system containing 4 to 28 wt.% W and 0.1 to 1.72% C were studied. Alloys containing 0.1 to 0.61% C and 9.39 to 24.9% W were single-phased (Fig.1) with the exception of the alloy containing 0.35% C and 19.65% W where traces of a eutectic in the cobalt solid solution boundaries were noted. With increase in carbon content, the solubility of  
Card 1/6 ✓

The Limits of the Single-Phase ...

S/180/61/000/001/011/015  
E021/E406

tungsten decreased. Fig.2 shows the cobalt corner of the ternary phase diagram. In the W-C-Ni system, all alloys with less than 0.25% carbon were single-phased. An alloy containing 0.5% C and 14.5 or 19.5% W showed traces of a second phase. With 24.5% W crystals of WC appeared after sintering, after melting carbon with traces of a eutectic (Ni phase + WC) along the grain boundaries. Fig.4 shows the phase diagram for this system. The solubility of tungsten bears little relation to the carbon content. Study of the limits of the two-phase region WC + Co in the W-C-Co system was carried with alloys containing 55, 30 and 10% cobalt. Alloys with 55% Co had the  $\eta$  phase present when the carbon content calculated from tungsten carbide was less than 4.58%. Excess carbon led to the formation of a three phase structure (Co phase + WC + C). Alloys containing 6.12 to 4.58% carbon (as tungsten carbide) were two-phased (WC + Co). Alloys with 30% Co were two-phased when the carbon content was 5.83 to 6.12% (as tungsten carbide). In this system the limit at which carbon appeared coincided with the geometric line Co-WC. Studies of the W-C-Ni system were carried out with alloys containing 55, 30, 15 and 10% Ni. The carbon-rich boundary in this case was below the

Card 2/6

The Limits of the Single-Phase ...

S/180/61/000/001/011/015  
E021/E406

geometric line Ni-WC. Traces of  $\eta_1$  phase were detected in samples containing 30% Ni and 5.11% C (as WC). The alloy containing 15% Ni had traces of  $\eta_1$  phase when 5.88% C (as WC) was present. The boundary between the 2-phase (WC + Ni) and the 3-phase (WC + Ni +  $\eta_1$ ) in the case of the alloy containing 10% Ni was at a C content (as WC) of 6.04 to 6.10%. Some magnetic measurements were also made. These confirmed the metallographic analysis. There are 4 figures, 7 tables and 5 references: 1 Soviet and 4 non-Soviet.

SUBMITTED: June 15, 1960

Card 3/6

The Limits of the Single-Phase ...

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E021/E406

Fig.1. Microstructure of an alloy containing 0.15% C, 19.85% W,  
remainder Co (x100).



Фиг. 1. Микроструктура сплава состава:  
0.15% C, 19.85% W, остальное Co (x100)

Card 4/6

22974

1.1600 also 1521,4016

S/180/61/000/003/002/012  
E021/E135

**AUTHORS:** Chaporova, I.N., and Shchetilina, Ye.A. (Moscow)

**TITLE:** The process of sintering and the structure of tungsten carbide - cobalt and tungsten carbide - nickel alloys with a carbon deficit

**PERIODICAL:** Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Metallurgiya i toplivo, 1961, No.3, pp. 37-41

**TEXT:** The process of sintering was studied using production conditions for sintering, i.e. the temperature was gradually increased up to the sintering temperature and the alloys were subsequently cooled at different rates. Alloys with 10, 15, 30 and 40 weight % cobalt (nickel) were prepared with different deficits of carbon. The amount of carbon was varied by additions of tungsten. In alloys containing 40% cobalt, sintered at temperatures below where a liquid phase appears, the  $\eta_1$  phase in the form of lakes was detected. It was found that lakes of  $\eta_1$  phase can be formed when a liquid phase appears during sintering if the quantity of liquid is insufficient for recrystallization of the  $\eta_1$  phase through the liquid. Thus, alloys containing 30% cobalt, with a

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S/180/61/000/003/002/012

The process of sintering and the .... E021/E135

carbon content in the tungsten carbide of 5.47 weight % and less, sintered at 1400 °C, have lakes of  $\eta_1$  phase, the size of which is greater than or equal to that of the tungsten carbide grains. With increasing carbon or cobalt content the  $\eta_1$  phase, which formed in the solid state, can completely dissolve in the liquid and is then reprecipitated during cooling in the form of coarse crystals. Fast cooling from high temperatures above the liquidus can result in a eutectic structure. With alloys containing 15 and 10% cobalt, lakes of  $\eta_1$  phase were observed after sintering at 1450 °C with carbon contents in the tungsten carbide of 5.88 and 5.94 weight % respectively. With increase in carbon content, crystals of  $\eta_1$  similar to those in the alloy containing 30% cobalt were observed. Further increase in carbon content in the 10% cobalt alloy resulted in  $\eta_1$  phase in a needle shaped or dendritic form in a lace-like pattern. With very low carbon deficit, the  $\eta_1$  phase can be precipitated at the tungsten carbide - cobalt boundary in the alloys containing 10, 15 and sometimes 30% cobalt. Investigations of the tungsten - carbon - nickel alloys gave similar results. In the alloy containing 30% cobalt, a carbon content in the tungsten carbide of 5.35 weight % or less resulted

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22974

S/180/61/000/003/002/012

The process of sintering and the ... E021/E135

in a fine precipitate of  $\eta_1$  phase in the cementing phase. When the investigations were carried out in a carburizing atmosphere, precipitate of  $\eta_1$  was observed in the central region, with none in the periphery. Some samples were so saturated with carbon that free graphite occurred. With increase in temperature to 1450 °C, grain growth of the tungsten carbide occurred. The investigations showed that the method of saturating alloys containing  $\eta_1$  phase with carbon used in production is fully proved and does not lead to marked changes in the tungsten carbide grain size.

There are 2 figures (15 microphotographs) and 7 references: 3 Soviet and 4 English. The English language references read as follows:

- Ref.1: J. Gurland. J. Metals, 1954, Febr., v. 6 No.12, Section 2, pp. 285-290.
  - Ref.2: L. Brownlee, R. Edwards, T. Raine. Powder Metallurgy, 1954, Group IV, p. 50 (The Iron and Steel Institute).
  - Ref.4: P. Rautala, J. Norton. J. Metals, 1952, Oct., v. 4, No.10, pp. 1045-1050.
  - Ref.7: J. Gurland. J. Metals, 1954, November, p. 1327.
- SUBMITTED: July 9, 1960  
Card 3/3

18.1152

1045

28874

S/180/61/000/004/012/020  
E193/E383

**AUTHORS:** Rybal'chenko, R.V., Tret'yakov, V.I. and  
Chaporova, I.N.

**TITLE:** The effect of tantalum carbide on the composition and  
properties of the cobalt phase in the titanium  
carbide-tungsten carbide-cobalt alloys

**PERIODICAL:** Akademiya nauk SSSR. Izvestiya. Otdeleniye  
tekhnicheskikh nauk. Metallurgiya i toplivo.  
no. 4, 1961, pp. 83 - 89

**TEXT:** The effect of TaC additions on the properties of WC-  
-TiC-Co and TiC-WC alloys has been frequently studied but there  
are no published data on the effect of this compound on the  
properties of the Co binder as present in the cemented WC-TiC  
carbides; hence the present investigation whose object was to  
determine the boundary of the single-phase region in the Co-rich  
corner of the TiC-WC-Co and TiC-WC-TaC-Co systems, the melting  
points of the eutectics formed in these systems, and microhardness  
of the Co-rich solid solution at room and elevated temperatures.  
In addition, the effect of excess (free) carbon on the properties  
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S/180/61/000/004/012/020  
E195/E385

The effect of tantalum carbide ....

of these alloys was also studied. The experimental alloys were prepared in the following manner: three TiC-TaC-WC alloys were prepared first by adding TaC to a  $\text{TiO}_2$  + WC + C mixture and heating the whole at 2 000 - 2 200 °C in hydrogen. The composition of these alloys is given below:

Alloy No.	Nominal composition, %		
	TiC	TaC	WC
1	28	5	67
12	28	11	61
24	22	22	56

After grinding and deoxidising, these alloys in the powder form were either sintered or melted with cobalt to form Co-TiC-TaC-WC alloys containing 10 - 99.8% Co. In some cases, excess carbon was introduced by melting the alloys in a graphite crucible. All

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alloys were examined after a homogenising treatment, consisting of 24 hours at 1 250 °C, followed by furnace-cooling. The results of hardness measurements are reproduced in Figs. 3 and 4.

In Fig. 3, the Vickers hardness ( $H_V$ , kg/mm<sup>2</sup>) is plotted against the test temperature ( $t$ , °C), the various curves relating to pure cobalt (Curve 6) and Co-base solid solutions containing TiC (Curve 1), TaC (Curve 2), TiC + WC (Curves 3, 4) and TiC + WC + TaC (Curve 5). In Fig. 4, the microhardness

( $H_\mu$ , kg/mm<sup>2</sup>) is plotted against the carbide content (wt.%) in Co-base solid solutions containing TiC (Curves 1, 2), TaC (Curve 3), TiC + WC (Curves 4, 5) and TiC + WC + TaC (Curves 6, 7); broken curves relate to alloys containing excess carbon. Several conclusions were reached:

1) addition of TaC (in quantities used in the present investigation) to a TiCWC solid solution does not affect the solubility of TiCWC in Co, irrespective of whether there is a deficiency or an excess of carbon in the system. The boundary of the solid

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solubility range in the Co-TiC-WC system is shown by the curve in the diagram reproduced in Fig. 1, where the concentration is in wt.%.  
 2) The 2-phase Ta-bearing alloys have the melting point of the binary eutectic (Co-TiWC-TaC) approximately 100 °C higher than the melting point of the corresponding eutectic in the Co-TiWC system. At the same time, the melting point of the ternary eutectic (Co + TiWC-TaC + C) is only 20 - 30 °C higher than that of the Co + TiWC + C eutectic.

3) Room-temperature hardness of the Co-TiWC-TaC single-phase alloys is higher than that of the corresponding Ta-free materials, this difference persisting up to 400 °C. This means that addition of TaC to cemented carbides should increase the high-temperature strength of the Co binder whereby the performance of these alloys in some applications should be improved. This, however, applies only to alloys containing no excess (free) carbon in the presence of which hardness of the TaC-bearing solutions decreases, although still remaining higher than that of TaC-free alloys. Hence the importance of a strict control of the  
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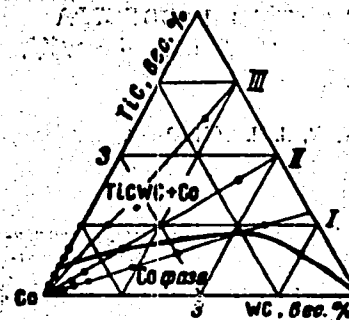
The effect of tantalum carbide .... E193/E383

carbon content in commercial-grade, Ta-bearing cemented carbides. L.Ye. Pivovarov and A.Ye. Koval'skiy participated in this work.

There are 4 figures, 3 tables and 7 references: 2 Soviet-bloc and 5 non-Soviet bloc. The English-language reference quoted in the abstract is: Ref. 4 - Miller - Metal Progr., 1953, 63, No. 4, 35.

SUBMITTED: July 22, 1960

Fig. 1:



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5

15 2240

24196  
S/129/61/000/007/011/016  
E073/E535

AUTHORS: Chaporova, I.N., Shchetilina, Ye. A. and Serebrova, O.I.  
TITLE: Influence of Additional Tempering on the Properties of  
the Carbides WC-Co

PERIODICAL: Metallovedeniye i termicheskaya obrabotka metallov,  
1961, No.7, pp.44-46

TEXT: The authors investigated the carbides BK4B (VK4V),  
BK6B (VK6V), BK8B (VK8V) and BK6M (VK6M) after heat treatment.  
The specimens were heated in a resistance furnace for 1.5-2 hours  
at 750, 500, 250 and 150°C. The duration of soaking at the  
tempering temperature was 2 hours and this was followed by cooling  
at a rate of 2°C/min. From each batch specimens were taken for  
investigating the microstructure, determining the coercive force,  
the bending strength and for the alloy VK4V also the impact  
strength. The specimens from the carbides VK8V, VK6V and VK4V  
contained micrographite inclusions in addition to grains of a  
tungsten carbide and veins of the cobalt phase. The alloy VK6M  
had a two-phase composition. Granulometric analysis of the  
carbide phase showed that during heat treatment (tempering at  
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various temperatures), the size of the tungsten carbide grains did not change either in the coarse grain carbides VK8V and VK4V, the medium grain carbide VK6V or in the fine grain carbide VK6M. The shape of the grains of the WC phase also did not change. No difference was observed in the coercive force values before and after tempering. A slight increase in the bending strength (by 8 to 10 kg/mm<sup>2</sup>) was observed after tempering at 250°C. However, tempering at 500 and 750°C did not result in any change of the bending strength. Taking into consideration the square errors of the mean arithmetic values, it can be stated that even at 250°C the influence of tempering is insignificant and is almost entirely overshadowed by fluctuations of the average strength values. Tempering of the alloy VK6V at 250 and 500°C showed no influence on the bending strength. In tests with a second batch of specimens of the same alloy, an appreciable drop in the strength was observed (by 23 and 21 kg/mm<sup>2</sup>, respectively) for both tempering temperatures. Tests of the alloy VK4V at 750, 500, 250 and 150°C revealed in all cases a very slight tendency to a drop in the bending strength (by 6 to 13 kg/mm<sup>2</sup>) which did not exceed

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E073/E535

the limits of the fluctuations of the average strength values. No difference was observed between the impact strength values of the carbide VK4V before and after tempering. Tempering of three different batches of the carbide VK6M was first carried out at 250, 500 and 750°C. In the batch tempered at 500°C, an appreciable increase in strength was observed, from 149 to 171 kg/mm<sup>2</sup>. For verifying this all the three batches were again tempered at 500°C. The strength of the specimens of both batches corresponded to the initial state and for the third batch the strength values differed from the average ones. The investigations have shown that tempering of the carbides VK4V, VK6V and VK8V at 750, 500, 250 and 150°C does not produce any appreciable change in the properties. The investigated carbides contain graphite inclusions and, in the presence of graphite, decomposition of the Co solution is made easier and the composition of the cementing phase in the alloys was near to that of pure cobalt. Apparently additional heating does not change the composition of the Co phase and, therefore, does not have any influence on the properties of the WC-Co alloys. The carried out experiments and the explanation of

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the obtained results cannot be considered exhaustive, since the changes in the properties of the alloys can be brought about by other factors (changes in the stress state of the alloy, phase transformations of the Co phase etc.). There are 1 figure, 2 tables and 3 references: 1 Soviet, 1 Austrian and 1 English: U.S. Patent No. 278073 (Method of heat treatment of carbide plates for increasing the tool service life).

[Abstractor's Note: This is an abridged translation.]

ASSOCIATION: Vsesoyuznyy Nauchno-Issledovatel'skiy institut  
tverdykh splavov (All Union Carbide Scientific  
Research Institute)

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15 2240

29531  
S/078/61/006/011/006/013  
B101/B147

AUTHORS: Rybal'chenko, R. V., Chaporova, I. N., ~~Tret'yakov, V. I.~~

TITLE: Effect of carbon on the solubility of titanium carbide in cobalt, and some properties of Ti-C-Co alloys

PERIODICAL: Zhurnal neorganicheskoy khimii, v. 6, no. 11, 1961, 2517-2527

TEXT: The ternary system Ti-C-Co has not been studied as yet. The authors studied the action of C on the solubility of TiC in the system TiC-Co. The following initial substances were used: Co obtained by calcinating cobalt oxalate and reducing the oxide by  $H_2$ ; TiC obtained by reduction of  $TiO_2$  by carbon black, and Ti metal. The components were fused in a vacuum furnace. Some samples were homogenized in  $H_2$  stream. The following alloys were synthesized: TiC-Co alloys with 0.2-10 % by weight of TiC<sub>0.98</sub>; with 0.6, 0.8, and 1.5 % of TiC<sub>0.93</sub> and alloys with TiC<sub>0.64</sub>, TiC<sub>0.55</sub>, and TiC<sub>0.50</sub>. Samples with C excess were obtained by

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Effect of carbon on the solubility...

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S/078/61/006/011/006/013  
B101/B147

melting in graphite crucibles. The alloys with 0.2 and 0.4 % of  $\text{TiC}_{0.98}$  as well as those with 0.6 and 0.8 % of  $\text{TiC}_{0.93}$  were single-phase. Alloys with a higher TiC content showed a  $\text{TiC} + \text{C}$  eutectic at the polyhedral faces of the Co phase. Alloys molten in  $\text{H}_2$  stream at  $1350-1450^\circ\text{C}$  showed decarbonization, due to which the solubility of TiC in Co and the melting point of the alloy increased. Microstructural analyses of the samples molten in the vacuum confirmed that the solubility of TiC in Co increases due to decreasing content of C. Samples molten in graphite crucibles showed that the solubility of TiC decreased to 50 %. For alloys saturated with C and having an excess of C, the solubility of TiC was not higher than 0.2 %. With decreasing C content it increased up to 5 %. Thermal analysis (determination of solidus points by an MOP-48 (MOP-48) pyrometer) showed that with rising TiC content melting temperature decreased from  $1480^\circ\text{C}$  to  $1360^\circ\text{C}$ . Melting point of the eutectic  $\text{TiC} + \text{Co}$  was  $1365^\circ\text{C}$  (measured by NN (PP) thermocouple). With decreasing C content it increased to  $1440^\circ\text{C}$ . X-ray analysis, performed by K. F. Kuznetsova and L. Kh. Pivovarov under supervision of A. Ye. Koval'skiy by an YPC-50 (URS-50) apparatus, showed that in pure cobalt alloys only cubic Co occurred; in cobalt alloys with 0.2-0.6 % of

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Effect of carbon on the solubility...

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TiC<sub>0.98</sub>, which also contained graphite, only hexagonal Co occurred. C-free alloys behaved differently: Up to a TiC content of 0.6 %, Co was cubic; with 1.5 % of TiC, Co was hexagonal. Microhardness determined by a PMT-3 (PMT-3) apparatus showed the following: For pure Co, microhardness was 250 kg/mm<sup>2</sup>; for 0.2 % of TiC, it increased to 275 kg/mm<sup>2</sup>, and this value did not change with further increasing TiC content. If the alloy contained graphite inclusions (Co + C eutectic), microhardness decreased to 200 kg/mm<sup>2</sup>. In alloys containing very little C the hardness of the Co phase increased to 300 kg/mm<sup>2</sup> due to increased solubility of Ti in Co. Change of hardness with rising temperature of solid solutions Co + TiC measured by a BWM-1 (VIM-1) apparatus showed a slight difference from the hardness of pure cobalt up to 300°C. At higher temperatures, pure Co is harder. It is evident that the presence of C considerably decreases the hardness of alloys. The melting point of the ternary eutectic TiC + C + Co is 1200°C. Therefore, the synthesis of TiC-Co alloys has to be performed such that rather a loss of C than enrichment by C takes place. Papers by V. N. Yeremenko (Zh. neorg. khimii, 1, 2131 (1956)),

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A. N. Zelikman and D. S. Bernshteyn (Tekhnologiya tsvetnykh metallov (Technology of nonferrous metals) Sbornik trudov, GONTI, M., 1952, v. 23, p. 48) are mentioned. There are 5 figures, 6 tables, and 10 references: 5 Soviet and 5 non-Soviet. The three most recent references to English-language publications read as follows: Max Hansen. Constitution of binary alloys, New York - Toronto - London, 1958; J. Cadoff, J. D. Nielsen, J. Metals, 5(212), 248 (1953); Nishimiro Hideo, Kimuro Hirozo. J. Japan Inst. Metals, 20, 528 (1956).

SUBMITTED: June 3, 1960

Card 4/4

15.2410

15.2240

33452

S/126/61/012/006/009/023  
E193/E383

AUTHORS: Baskin, M.L., Tret'yakov, V.I. and Chaporova, I.N.  
TITLE: Diffusion of niobium in titanium carbide and in the  
TiC-NbC solid solution of equimolecular composition  
PERIODICAL: Fizika metallov i metallovedeniye, v.12, no. 6,  
1961, 860 - 864

TEXT: The object of the present investigation was to obtain data on diffusion of Nb in titanium carbide and in the TiC-NbC alloy, indispensable in solving the problems arising in studies of processes taking place during the preparation of so-called complex carbides. To facilitate sintering of TiC specimens, 0.25% Ni was added to the powder mixture, the Ni binder volatilizing completely during subsequent sintering. Sintering of both TiC and TiC-NbC specimens (15 mm diameter, 5 mm thick) was carried out in vacuum in two stages: slow heating (10 °C/min) to about 1 930 °C, followed by 2.5 hours at 2 300 °C (a high sintering temperature was used to ensure that no grain growth would occur during the subsequent diffusion anneals carried out at temperatures below 2 300 °C. The properties of Card 1/3

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S/126/61/012/006/009/023  
E193/E383

sintered compacts are given in Table 2. The method employed for determination of the diffusion coefficients,  $D$ , entailed deposition of thin, radioactive  $Nb^{95}$  films on one side of polished specimens, and measuring the counting rates on the opposite side as a function of time at the test (diffusion annealing) temperature. The results (average of four measurements) for the diffusion of Nb in TiC are given in Table 3, those for diffusion of Nb in TiC-NbC alloy being given in Table 4. The variation of  $D$  in the former and latter cases can be described by:

$$D = 2.4 \exp\left(-\frac{84\,000}{RT}\right) \text{ cm}^2/\text{sec} \quad (4)$$

and:

$$D = 4.7 \times 10^2 \exp\left(-\frac{120\,000}{Rt}\right) \quad (5)$$

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Diffusion of niobium ....

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the two values of 84 000 and 120 000 representing the activation energies (cal/mole) for the respective processes. The results obtained showed that addition of NbC to TiC decreases considerably the rate of diffusion of Nb, which indicates that the atomic-bond forces in the TiC-NbC solid solution are higher than those in TiC. Acknowledgments are expressed to L.G. Grigorenko and N.S. Anikina, technicians. There are 3 figures, 4 tables and 7 references: 6 Soviet-bloc and 1 non-Soviet-bloc.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov (All-Union Scientific Research Institute of Hard Alloys)

SUBMITTED: January 24, 1961

Card 3/10 3

TRET'YAKOV, Vsevolod Ivanovich. Prinimali uchastiye: CHAPOROVA, I.N.,  
kand. tekhn. nauk; KOVAL'SKIY, A.Ye., kand. khim. nauk;  
BARANOV, A.I., inzh.; MEYERSON, G.A., prof., doktor tekhn.  
nauk, retsenzent; IVENSEN, V.A., kand. tekhn. nauk, retsenzent;  
BABICH, M.M., inzh., retsenzent; OL'KHOV, I.I., red.; MISHARINA,  
K.D., red. izd-va; DOBUZHINSKAYA, L.V., tekhn. red.

[Ceramic-metal hard alloys; physicochemical principles of their  
production, properties and fields of use] Metallokeramicheskie  
tverdye splavy; fiziko-khimicheskie osnovy proizvodstva,  
svoistva i oblasti primeneniia. Moskva, Gos.nauchno-tekhn.izd-  
vo lit-ry po chernoi i tsvetnoi metallurgii, 1962. 592 p.

(MIRA 15:1)

(Ceramic metals)

Investigation of the effect ....

S/126/62/013/005/008/031

E193/E383

carried out at 400 °C on specimens vacuum-annealed for 1 hour at temperatures varying from 1 000 - 2 300 °C. The structure of the fracture surfaces of specimens broken under impact at room temperature was examined with the aid of an electron microscope, both optical and electron microscopes being used for the examination of microstructure. The results can be summarized as follows:

1) the mechanical properties of cast and cold-worked tungsten were not affected by annealing at temperatures below 1 200 °C, the average numerical values obtained being:

UTS = 62 kg/mm<sup>2</sup>; Brinell hardness number HB = 430; elongation  $\delta$  = 17%; reduction in area  $\psi$  = 50%.

2) After annealing at temperatures equal to or higher than 1 600 °C, the UTS of the metal studied decreased to ~ 20 kg/mm<sup>2</sup> and its HB to ~300. In contrast to the general rule, the decrease in hardness was not accompanied by a corresponding increase in plasticity. On the contrary, both  $\delta$  and  $\psi$  decreased after this treatment, the former to about 3% and the latter to about 18%.

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Investigation of the effect .... S/126/62/013/005/008/031  
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- 3) Irrespective of annealing temperature, no evidence was found of the precipitation of a second-phase at the grain boundaries of recrystallized specimens.
  - 4) Recrystallization of tungsten was accompanied by broadening of the grain boundaries and by a gradual increase in the degree of order of the structure in the interior of the grains (this latter effect was revealed by the fact that small etching pits which were randomly oriented on deformed material formed a regular pattern on recrystallized specimens).
  - 5) The width of grain boundaries depended on the degree of misalignment between the adjacent grains and increased with increasing annealing temperature, reaching a value of 3.5 - 4.5  $\mu$  in cast material, which can be regarded as material annealed at a temperature just below the melting point of the metal.
  - 6) Plastic deformation caused considerable changes in the structure of the interior of the grains and promoted the formation of a specific microstructure, characterized by very narrow (0.5 - 1  $\mu$ ) grain boundaries.
  - 7) The decrease in plasticity of recrystallized tungsten was
- Card 3/4

Investigation of the effect ....

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found to be directly related to the broadening of grain boundaries. This was taken to indicate that the brittleness of recrystallized tungsten and other similar metals was caused by intergranular internal adsorption of impurities. In view of the results obtained it would appear that there are four possible ways of minimizing the embrittling action of recrystallization of tungsten and other metals prone to this effect: a) reducing the impurity content of the metal; b) grain refinement; c) heat-treatment; d) alloying with elements inhibiting intergranular internal adsorption and harmful impurities. That the last of these methods may be no less effective than the first is indicated by the results of many investigations carried out by V.I. Arkharov and his co-workers and by the fact that the plasticity of W and Mo can be increased considerably by the addition of 20 - 35% rhenium in the former and 40 - 50% rhenium in the latter case. There are 4 figures.

SUBMITTED: August 15, 1961

Card 4/4

41520

S/126/62/014/003/011/022  
E202/E492

21.2400

AUTHORS: Baskin, M.L., Tret'yakov, V.I., Chaporova, I.N.

TITLE: Diffusion of tungsten in monocarbides of tungsten tantalum, titanium, and in solid solutions of TiWC and TiWCTaC

PERIODICAL: Fizika metallov i metallovedeniye, v.14, no.3, 1962, 422-427

TEXT: Diffusion coefficients of tungsten (D), and activation energies (Q), during the diffusion of W in TiC, WC, TaC and in solid solutions comprising: 93% TiC + 7% WC; 77% TiC + 23% WC; 59% TiC + 34% WC + 7% TaC and 48% TiC + 37% WC + 15% TaC (all % mol), were determined. A method of introducing and anchoring on the surface of the sample radioactive tungsten was developed. Considerable difficulties were experienced in compacting and high temperature diffusional annealing. Chemical composition including combined and free and the stoichiometric C content, lattice parameter of the original constituents and their origin were given as well as the details of the compacts. The latter included specific gravity, lattice parameter, porosity. Card 1/2

Diffusion of tungsten ...

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E202/E492

grain size and Ni content (spectrometrically). L. Foster's method (J. Amer. Ceramic Soc., v.33, no.1, 1950, 27) of compacting was used throughout. D values for the diffusional annealing at 2130, 2170, 2230 and 2300°C were determined for all the above compositions and the Q and D<sub>0</sub> values calculated therefrom. It was found that TiC had the lowest Q (115 ± 8 kcal/mol) while 50% TiC + 34% WC + 7% TaC had the highest (225 ± 27 kcal/mol). Addition of TaC to the solid solution of TiCWC substantially increased Q. Certain compositions of TiCWC and TiCWCTaC showed maximum values of Q. The presence of these maxima were explained by the energy levels and the incomplete 3d shell in titanium. There are 4 tables.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov (All Union Scientific Research Institute of Hard Alloys)

SUBMITTED: December 26, 1961

Card 2/2

BASKIN, M.L.; TRET'YAKOV, V.I.; CHAPOROVA, I.N.; Prinimali uchastiye:  
ANIKINA, N.S.; GRIGORENKO, L.G.; CHEREDINOV, A.A.

Diffusion of tungsten in monocarbides of tungsten, tantalum,  
and in TiWC and TiWC-TaC solid solutions. Fiz. met. i  
metalloved. 14 no.3:422-427 S '62. (MIRA 15:9)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh  
splavov.

(Tungsten) (Diffusion)



BASKIN, M.L.; TRET'YAKOV, V.I.; CHAPOROVA, I.N.

Niobium diffusion in titanium carbide in a solid solution of TiC-NbC of equimolar composition. Fiz. met. i metalloved. 12 no.6: (MIRA 16:11)  
860-864 D '61.

1. Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov.

1. 25275-65 ENG(j)/EWP(e)/EWT(m)/EPT(c)/EWA(d)/EPR/EWP(t)/EWP(b) Pr-4/Ps-4  
 IJP(c) MJW/JD/WW/JG/WH  
 ACCESSION NR: AR4048251 S/0137/64/000/009/I086/I086 39  
 38  
 E

SOURCE: Ref. zh. Metallurgiya, Abs. 9I556

AUTHOR: Rysbal'chenko, R. V.; Tret'yakov, V. I.; Chaporova, I. N.

TITLE: The effect of structurally free carbon on certain  
 physicomachanical and performance properties of titanium-tungsten  
hard alloys 27 21

CITED SOURCE: Sb. tr. Vses. n.-i. in-t tverdykh splavov, no. 5,  
 1964, 173-181

TOPIC TAGS: titanium base alloy, tungsten containing alloy, metal  
 physical property, metal mechanical property, carbon alloy T5K10,  
alloy T15K6, alloy T30K4 4

TRANSLATION: The following methods were used in investigating the  
 alloys: chemical, metallographic, determination of specific weight,  
 sigma<sub>0.2</sub> at room temperature and at 800°, resistance to wear during  
 cutting, electrical conductivity, and measurement of RA and H<sub>0.2</sub>. When  
 sintering T5K10, T15K6 and T30K4 alloys in carbonized packing (pure

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L 25275-65

ACCESSION NR: AR4048251

korraaks, korraaks +0.05% carbon, graphitic sandstone, graphitic sandstone with carbon black, and lamp black) the amount of bound carbon does not change. The amount of free carbon increases gradually up to the saturation point of the cobalt phase at sintering temperature. In the presence of structurally free carbon (graphite) in the alloys investigated,  $\sigma_{bu}$ , in comparison to samples sintered in korraaks and which do not contain graphite, increases to 20-25 kg/mm<sup>2</sup> at 20°, while at 800° the same samples have the lowest value of  $\sigma_{bu}$ . The wear resistance of T15K6 and T5K10 alloys during steel cutting decreases with an increase in the level of free carbon, while for alloy T30K4 it is almost unchanged.

SUB CODE: MM

ENCL: 00

Card 2/2

L 40056-66 EWT(m)/EWP(t)/ETI IJP(c) WH/JW/JD

ACC NR: AP6025942

SOURCE CODE: UR/0226/66/000/007/0076/0083

AUTHOR: Chaporova, I. N.; Rybal'chenko, R. V.; Vrzheshch, Ye, Ya.

ORG: All-Union Scientific Research Institute of Hard Alloys (Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov)

TITLE: Synthesis and properties of (Ti, W, Cr)C carbides <sub>27 27 27</sub> 27

SOURCE: Poroshkovaya metallurgiya, no. 7, 1966, 76-83

TOPIC TAGS: sintering, ~~sintered carbide~~, titanium, carbide, tungsten carbide, chromium carbide, ~~carbide structure~~, ~~carbide property~~

ABSTRACT: The effect of adding up to 25%  $Cr_3C_2$  on the properties of (Ti, W)C carbide with a constant TiC:WC ratio of 35:65, was investigated. The initial (Ti, W, Cr)C carbides were synthesized from  $TiO_2 + WC + Cr_2O_3 + C$  powders in hydrogen at temperatures from 2573 K for pure  $TiO_2 + WC$  to 1923 K for carbide with 25%  $Cr_3C_2$ . The carbide powders were compacted and sintered in vacuum at 2073—2123 K. The porosity of sintered compacts did not exceed 0.2%. An x-ray diffraction analysis<sup>1</sup> revealed that all the alloys have a solid-solution structure with an fcc lattice. With increasing  $Cr_3C_2$  content oxidation resistance sharply increased. The respective weight loss of (TiW)C carbide and carbide containing 20%  $Cr_3C_2$  was 72 and 3.6% of the original weight in 10 hr at 1270 K. At 20%  $Cr_3C_2$ , the resistivity increased by 60%, Young's modulus dropped from 37 to 33  $n/m^2 \cdot 10^{10}$ . With increasing temperature from

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